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HIGH-VOLTAGE-STABLE ELECTROLYTES FOR
 $Li_{1+x}Mn_2O_4$ / CARBON SECONDARY BATTERIES

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BACKGROUND OF THE INVENTION

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This invention relates to non-aqueous electrolyte compositions for secondary (rechargeable) lithium battery cells and, more particularly, to electrolyte compositions that are capable of resisting decomposition normally resulting from oxidation which occurs in $Li_{1+x}Mn_2O_4$ / carbon cells during recharging under conditions of greater than about 4.5 V or 55°C.

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The advantages generally provided by rechargeable lithium batteries are often significantly overshadowed by dangers of the reactivity of lithium in cells which comprise lithium metal as the negative electrode. A more advanced and inherently safer approach to rechargeable lithium batteries is to replace lithium metal with a material capable of reversibly intercalating lithium ions, thereby providing the so-called "rocking-chair" battery in which lithium ions "rock" between the intercalation electrodes during the charging/recharging cycles. Such a Li metal-free "rocking-chair" battery may thus be viewed as comprising two lithium-ion-absorbing electrode "sponges" separated by a lithium-ion conducting electrolyte usually comprising a Li^+ salt dissolved in a non-aqueous solvent or mixture of such solvents. Numerous such salts and solvents are known in the art, as evidenced in Canadian Patent Publication No. 2,022,191, dated 30 January 1991.

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The output voltage of a rechargeable lithium battery cell of this type is determined by the difference between the electrochemical potential of Li within the two intercalation

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electrodes of the cell. Therefore, in an effective cell the positive and negative electrode materials should be able to intercalate lithium at high and low voltages, respectively. Among the alternative materials that can effectively replace lithium metal as the negative electrode, carbon provides the best compromise between large specific capacity and good reversible cycling behavior. Such use of carbon, however, presents some detractions, such as loss of average output voltage and energy density, as compared to lithium metal, since the voltage of a Li_xC_6 negative electrode is always greater than that of a pure lithium negative electrode.

To compensate for the loss of voltage associated with the negative electrode, a strongly oxidizing intercalation material is preferably used as the positive electrode. Such an electrode material is the spinel phase $\text{Li}_{1+x}\text{Mn}_2\text{O}_4$, usually combined with a small amount of carbon black to improve electrical conductivity and provide the practical composite electrode, that can reversibly intercalate lithium at a voltage of 4.1 V vs. Li. Use of such a strongly oxidizing intercalation material as positive electrode, however, introduces a further concern, namely, the risk of electrolyte decomposition from oxidation at the higher operating voltages, i.e. greater than about 4 V. For instance, since the voltage of the $\text{Li}_{1+x}\text{Mn}_2\text{O}_4$ / Li couple is about 4.1 V, one should charge the cell up to a voltage of about 4.5 V in order to take full advantage of this redox system. As a result, the electrolyte in such a cell must be stable over a voltage window extending above 4.5 V to about 5.0 V. Also, when used in the noted "rocking chair" cells, the electrolyte compositions must be stable down to about 0 V with respect to a composite carbon negative electrode, e.g., petroleum coke combined with about 1-5% of each of carbon black (Super-S) and an inert binder.

Presently-used intercalation electrolytes, e.g., a 1M solution of LiClO_4 in a 50:50 mixture of ethylene carbonate (EC) and diethoxyethane (DEE) such as described in U.S. Pat.

No. 5,110,696, when employed in a $\text{Li}_{1+x}\text{Mn}_2\text{O}_4$ / C cell, will begin to oxidize at about 4.5 V at room temperature and as low as about 4.3 V at temperatures in the range of 55°C. Thus, to operate such a cell in the higher temperature ambient, one must reduce the charging cut-off voltage to a level below about 4.3 V in order to avoid electrolyte oxidation. Because of this lower cut-off voltage, the available capacity of the cell at about 55°C is only 75% of that at room temperature.

When cells comprising these previously-available electrolytes are cycled to a voltage even slightly greater than 4.3 V, electrolyte oxidation occurs. Although small, this oxidation can jeopardize the capacity, cycle life, and safety of the battery cell. For example, the electrode oxidation reaction consumes part of the charging current which is then not recovered when discharging the cell, resulting in a continuous loss in the cell capacity over subsequent cycles. Further, if during each charge a small part of the electrolyte is consumed, excess electrolyte must be included when the cell is assembled. This in turn results in less active material for a constant volume battery body and consequently less initial capacity. In addition, the oxidation of the electrolyte often generates solid and gaseous byproducts, the solid of which build up a passivating layer on the particles of the active material, increasing the polarization of the cell and lowering the output voltage. Simultaneously, and more importantly, the gaseous byproducts increase the internal pressure of the cell, thereby increasing the risk of explosion and leading to unsafe and unacceptable operating conditions.

SUMMARY OF THE INVENTION

The present invention provides a class of electrolyte

compositions that is exceptionally useful for minimizing electrolyte decomposition in secondary batteries comprising strongly oxidizing positive electrode materials. These electrolytes are thereby uniquely capable of enhancing the 5 cycle life and improving the temperature performance of practical "rocking chair" cells. In our search for such an effective electrolyte, we examined literally hundreds of compositions, since the catalytic activity of the desirable positive electrode materials can not be predicted. As a 10 result of these extensive investigations, we have discovered a group of electrolyte compositions whose range of effective stability extends up to about 5.0 V at 55°C, as well as at room temperature (about 25°C.).

15 In selecting an improved electrolyte, a number of basic essential factors are considered. Ideally, the temperature range of fluidity should be broad, the ionic conductivity should be high, and the charging cut-off voltage which avoids electrolyte oxidation should be high. In our 20 selection process, the fluid temperature ranges of the compositions, i.e., between the melting and boiling points, were determined, respectively, with a differential scanning calorimeter (Perkin-Elmer Model DSC-4) and by thermometry in a common laboratory reflux apparatus. Next, the ionic conductivity of the different electrolyte compositions was 25 measured over a wide practical temperature range (-25°C to 65°C) using a high frequency impedance analyzer (Hewlett 30 Packard Model HP4129A, 5 Hz - 10 MHz). Finally, the stability of the electrolytes against oxidation was determined over varying temperature and charging voltage ranges by means of a potentiostatic mode coulometer (CNRS, Grenoble, France, Model "Mac-Pile", version A-3.01e/881) 35 using a LiMn_2O_4 electrode to simulate activity to be expected in a practical cell. From these determinations, we have discovered that the above-noted exceptional electrolyte results are obtained from a composition of about a 0.5M to 2M 40 solution of LiPF_6 , or LiPF_6 to which up to about an equal amount of LiBF_4 has been added, dissolved in a mixture of

dimethylcarbonate (DMC) and ethylene carbonate (EC) wherein these solvent components are present in the weight percent ratio range from about 95 DMC:5 EC to 33 DMC:67 EC. A preferred ratio of these solvents is from about 80 DMC:20 EC to 20 DMC:80 EC.

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THE DRAWING

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The present invention will be described with reference to the accompanying drawing of which:

10 FIG. 1 depicts a plot of cell current against charging voltage at room temperature for a secondary cell comprising a positive Li intercalation electrode and an electrolyte of LiClO_4 in 50:50 EC:DEE;

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15 FIG. 2 depicts comparative plots of cell current against charging voltage at room temperature and at 55°C for secondary cells comprising a positive Li intercalation electrode and an electrolyte of LiClO_4 in 50:50 EC:DEE;

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20 FIG. 3 depicts comparative plots of cell current against charging voltage at room temperature for secondary cells comprising a positive Li intercalation electrode and respective electrolytes of LiClO_4 in 50:50 EC:DEE and LiPF_6 in 67:33 DMC:EC; and

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25 FIG. 4 depicts comparative plots of cell current against charging voltage at 55°C for secondary cells comprising a positive Li intercalation electrode and respective electrolytes of LiClO_4 in 50:50 EC:DEE and LiPF_6 in 67:33 DMC:EC.

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DESCRIPTION OF THE INVENTION

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Our investigations covered the vast range of combinations of currently known Li-bearing electrolyte salts and non-aqueous solvents, and the more commonly employed positive intercalation electrode materials. The salts included LiAsF_6 , LiBF_4 , LiCF_3SO_3 , LiClO_4 , $\text{LiN}(\text{CF}_3\text{SO}_2)_2$, and LiPF_6 . The solvents included diethylcarbonate, diethoxyethane, dimethylcarbonate, ethylene carbonate, and propylene carbonate. The test electrode compositions comprised LiCoO_2 , LiMn_2O_4 , LiNiO_2 , MnO_2 , and V_2O_5 .

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The initial scanning of melting to boiling ranges of solutions of the various salts in the solvents and mixtures thereof indicated that 1M to 2M solutions provided generally good utility from about -40°C to 130°C . Subsequent testing for effective electrolytes was conducted with these solutions in the projected battery cell "working range" of about -25°C to 65°C .

Screening of the important ionic conductivity property of the candidate electrolytes indicated a widely disparate range of about 3 to 12 mS (millisiemens or millimohs) per cm. From an evaluation of the efficacy of a prior functional "rocking chair" battery electrolyte composition comprising a 1M solution of LiClO_4 in a 50:50 percent ratio mixture of ethylene carbonate and diethoxyethane, a minimum threshold conductivity for this selection process was set at about 10 mS/cm. Upon this criterion, the list of prospective candidate compositions rapidly narrowed to those comprising the solvent combination of dimethylcarbonate and ethylene carbonate. Further, the salt components were limited to LiPF_6 and some mixtures of LiPF_6 and LiBF_4 .

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The ultimate series of tests was conducted on these remaining compositions to determine their ability to

withstand oxidation (decomposition) under recharging voltages in excess of about 4.5 V. The CNRS "Mac-Pile" data acquisition system was operated in the potentiostatic mode at a scan rate of 40 mV/hr to test candidate electrolyte compositions against 10mg, 1 cm² samples of selected electrode material. This enabled the continuous plotting of coulometric measurements of charging voltage against cell current. From such curves the onset of electrolyte oxidation can be readily identified. This procedure can be seen with reference to FIG. 1 which plots the characteristic curve for the mentioned prior LiClO₄ / EC + DEE electrolyte at 25°C. The peaking at about 4.05 and 4.15 V vs. Li corresponds to the reversible removal of Li from the spinel structure of a LiMn₂O₄ positive cell electrode, while the rapid non-reversing increase in current beginning at about 4.5 V vs. Li heralds the onset of electrolyte oxidation at that charging level.

The effect of cell operating temperature is also indicated from such plots, as can be observed from FIG. 2 which depicts results of a test of the prior LiClO₄ electrolyte solution at the higher end of the ambient temperature range, about 55°C. With the dotted room temperature curve of FIG. 1 as a reference, one may readily see that the kinetics governing the electrolyte oxidation reaction lead to a lower electrolyte breakdown voltage as a result of increased temperature. The initiation of electrolyte oxidation at about 4.3 V vs. Li, and at even lower voltage during later recharge cycles, indicates that the charging cut-off voltage must be limited to about 4.1 V vs. Li for practical operation at the higher temperature. As a result of this limitation, the available cell capacity is, at best, only about 75% of that at room temperature.

From this electrolyte oxidation screening, we have discovered that an exceptional, wide temperature range, oxidation resistant electrolyte for a LiMn₂O₄ positive electrode intercalation battery cell, particularly one

21 utilizing the preferred $\text{Li}_{1+x}\text{Mn}_2\text{O}_4$ ($0 < x < 1$) electrode, may
 be realized in a 0.5M to 2M solution of LiPF_6 , or LiPF_6 with
 up to about an equal amount of LiBF_4 added, in a mixture of
 5 dimethylcarbonate (DMC) and ethylene carbonate (EC) within
 the weight percent ratio range from about 95 DMC:5 EC to
 20 DMC:80 EC. In a preferred such electrolyte solution the
 solvent ratio range is about 80 DMC:20 EC to 20 DMC:80 EC.
 An optimum composition for operation at room temperature and
 10 below is an approximately 1M LiPF_6 solution in a solvent
 mixture of about 33 DMC:67 EC, while a battery operating at
 higher temperatures in the range of 55°C optimally utilizes
 an electrolyte consisting essentially of an approximately
 15 1.5M LiPF_6 solution in a solvent combination of about
 67 DMC:33 EC. An additionally useful electrolyte consists
 20 essentially of an approximately 1M to 2M solution of equal
 parts of LiPF_6 and LiBF_4 in a solvent mixture of about
 25 50 DMC:50 EC.

20 The outstanding oxidation resistant characteristics
 of the preferred electrolyte compositions may be observed,
 with reference to the earlier-noted LiClO_4 composition, in
 FIG. 3 at room temperature and in FIG. 4 at 55°C. The
 negligible current increase, after the reversible Li
 intercalations, at voltages up to about 5 V vs. Li indicates
 25 this remarkable stability which enables enhanced cell
 capacity not only in the "rocking chair" cells comprising
 negative electrodes of carbon, e.g., petroleum coke, but also
 in Li negative electrode cells. Such a lithium metal cell
 utilizing a $\text{Li}_{1+x}\text{Mn}_2\text{O}_4$ positive electrode may be reasonably
 30 expected to achieve normal operating ranges of about 4.3 to
 5.1 V.

35 The efficacy of the new electrolyte compositions was
 confirmed in common Swagelock cell recycling tests. For
 example, test cells were assembled with positive electrodes
 comprising $\text{Li}_{1+x}\text{Mn}_2\text{O}_4$ which, according to usual practice,
 typically included about 3-10% carbon (Super-S graphite) to
 improve electrical conductivity and about 1-5% of an inert

14 binder, such as polytetrafluoroethylene. In the course of these test we noted that it was preferable to favor lower
5 carbon content in the range of about 4-7%, since the electrolyte oxidation tendency was additionally reduced. A
H set of such test cells with the separator element comprising
10 an electrolyte of 1 M LiPF₆ in 95 DMC:5 EC and a carbon (graphite or petroleum coke) negative electrode were repeatedly charged and discharge over two hours cycles at about 25°C and 55°C and at charging cut-off voltages of 4.9 V
15 and 4.5 V, respectively. Even at this cycling rate and high charging voltage, the voltage polarization was unusually small, confirming the high ionic conductivity of the electrolyte, and there was no significant loss of cell capacity, verifying the high voltage stability of the
electrolyte. The ability of the electrolyte to extend the cycle life of the batteries was amply demonstrated by the remarkable fact that the cell capacities after 500 cycles was only about 10% less than after 5 cycles.

20 The electrolyte solutions we have discovered may be employed in practical batteries with any of the various immobilizing means that have found utility in prior cells. In addition to being used to saturate the porous separator elements normally disposed between the cell electrodes, these new electrolytes solutions may be included in the form of
25 gelled or thickened compositions or they may be introduced into polymeric matrices as a secondary plasticizer. Such applications and other variants of this type will be apparent to the skilled artisan and are intended to be nonetheless included within the scope of the present invention as recited
30 in the appended claims.